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(54) Title: BATTERY CELL CHARGING SYSTEM HAVING VOLTAGE THRESHOLD AND BLEEDER CURRENT GENERATING CIRCUITS

(57) Abstract: A balanced battery cell charging circuit is provided. The circuit includes a comparator for comparing the voltage of a battery cell to a predetermined threshold voltage. If the cell voltage exceeds the threshold value, a bleeder current is generated. In one preferred embodiment, the bleeder current is subtracted from the charging current. In another embodiment, the bleeder current is multiplied, and the multiplied bleeder current is subtracted from a total charging current supplied to the cell. To control the charger circuit, current feedback is provided by monitoring the bleeder current generated against a maximum bleeder current, and adjusting the charging current accordingly. The topology of the present invention provides active cell balancing between cells of a battery, and low total power dissipation of the circuit.

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BATTERY CELL CHARGING SYSTEM HAVING VOLTAGE THRESHOLD
AND BLEEDER CURRENT GENERATING CIRCUITS

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a balanced battery cell charging circuit. More particularly, the present invention relates to a battery charging circuit that monitors the voltage of each cell within the battery, and supplies a charging current depending on the cell voltage. Particular utility of the present invention is a battery charging circuit for portable electronic devices; although the present invention has utility in any system that uses rechargeable batteries.

2. Description of Related Art

Various charger circuits and techniques for charging and recharging secondary cells are known. In one such technique, the cell voltage is monitored and a charge current supplied to the cell is reduced as the cell voltage increases. This technique is based on a recognition that, as the voltage across the cell increases, its charge acceptance decreases. Other battery charging techniques utilize circuitry for sensing the charge accepted by the cell and reducing the charge current supplied to the cell as the accepted charge decreases. In still another battery charging technique, a constant current is supplied to the cell during a first charging interval and a constant voltage is provided to the cell during a second charging interval. The first and second intervals may have predetermined durations or alternatively, may be a function of a battery condition, such as the cell voltage.

As is apparent, many battery charging techniques require measurement of the voltage across the rechargeable cell. Another reason for measuring the cell voltage is to prevent cell damage due to an overvoltage or undervoltage condition. More particularly, certain types of non-aqueous electrolyte battery cells, such as lithium ion cells, are susceptible to damage if charged to too high a voltage or permitted to be discharged to too low a voltage.

Secondary cells are often connected in series to power a load, since the total voltage across the string of series-connected cells is approximately equal to the sum of the voltages across each individual cell. One way to measure the individual cell voltages in a string of series-connected cells is to measure the total voltage across the

1 string of cells and divide the measured voltage by the number of cells. However, this
2 technique provides only a rough approximation of the individual cell voltage since
3 typically, the voltage across each cell varies somewhat.

4 Another technique for measuring the voltage across individual series-
5 connected cells is to provide a sensing circuit for each such cell and average the
6 outputs of the sensing circuits. For example, a plurality of differential amplifiers may
7 be provided, with input terminals of each amplifier coupled across a respective cell
8 and the output signals of the amplifiers averaged. However, since such a measurement
9 is of the average cell voltage, when using the measurement to control cell charging,
10 some cells will be overcharged and others will be undercharged in accordance with
11 the deviation between their respective voltage and the average measured voltage.
12 Moreover, use of plural sensing circuits results in disadvantageous component
13 duplication and concomitant increases in manufacturing time and cost.

14 One attempt to solve these attendant problems can be found in U.S Patent No,
15 5,652,501. This patent discloses battery charger/monitor circuit for charging and/or
16 monitoring a plurality of series-connected cells. The disclosed circuit includes a
17 voltage sensor for sensing the voltage across each of the cells to provide a high cell
18 voltage signal proportional to the highest voltage across any of the cells and a low cell
19 voltage signal proportional to the lowest voltage across any of the cells. The circuit is
20 operable in a monitor mode or a charge mode. In the monitor mode, the cells are
21 disconnected from a load if the low cell voltage signal decreases to a first
22 predetermined level. The circuit also includes a controller that provides a control
23 signal in response to the high cell voltage signal, the low cell voltage signal and a
24 current sense signal, for controlling the charging of the cells. In the charge mode, the
25 cells receive a constant charge current until the high cell voltage signal reaches a
26 second predetermined level, after which the voltage across the cell charged to the
27 highest voltage is held substantially constant, causing the charge current to be
28 reduced.

29 While this alleviates some of the attendant problems associated with the prior
30 art, this attempt does not provide a circuit that considers power dissipation criteria.
31 For IC implementation, there is often a limit as to the maximum power that the IC is
32 permitted to dissipate. Also, for portable device applications, it is necessary to be

1 very power conscious, for obvious reasons. In the aforementioned patent, the
2 disclosed topology reduces the cell voltage once a predetermined threshold is met.
3 However, this cannot accurately monitor power dissipation considerations, nor can
4 charging current be adjusted at a battery cell level.

5 SUMMARY OF THE INVENTION

6 Accordingly, the present invention solves the aforementioned drawbacks of
7 the prior art by providing a battery charging circuit that monitors the voltage of each
8 cell within the battery, and supplies a charging current depending on the cell voltage.
9 Unlike the aforementioned prior art references, the present invention controls the
10 battery the current supplied to each battery cell, based on a cell voltage tolerance.
11 Based on the cell voltage parameters, a bleeder current is generated which is
12 subtracted from the charging current, thereby reducing the total charging current
13 delivered to the cell. Additionally, the present invention provides a circuit that
14 minimizes power dissipation by generating a minimal bleeder current, multiplying the
15 bleeder current, and bleeding the multiplied bleeder current from the cell.

16 In one embodiment, the present invention provides a battery cell charging
17 circuit that includes a charger circuit supplying a charging current to said battery cell.
18 A comparator is used for comparing a battery cell voltage to a predetermined
19 threshold cell voltage. The comparator controls the generation of a bleeder current
20 proportional to the amount the battery cell voltage exceeds the predetermined
21 threshold. The bleeder is subtracted from the charging current supplied to the battery
22 cell.

23 In method form, the present invention provides method for charging a battery,
24 including the steps of supplying a charging current to a battery cell; comparing the
25 battery cell voltage to a predetermined threshold cell voltage; generating a bleeder
26 current if the cell voltage exceeds said predetermined threshold cell voltage; and
27 subtracting the bleeder current from the charging current.

28 In another preferred embodiment, the present invention provides a battery cell
29 charging circuit that comprises a battery including a plurality of cells. A charger
30 circuit supplies a charging current to each cell. A first comparator compares a battery
31 cell voltage to a predetermined threshold cell voltage, the comparator also controls the
32 generating a bleeder current proportional to the amount the battery cell voltage

1 exceeds the predetermined threshold. A current mirror generates the bleeder current
2 and a multiple of the bleeder current, the multiple of the bleeder is subtracted from the
3 charging current supplied to the battery cell. A second comparator is provided for
4 comparing the bleeder current to a maximum allowable bleeder current value, and
5 generating a feedback signal to the charger circuit to control the value of the charging
6 current.

7 It will be appreciated by those skilled in the art that although the following
8 Detailed Description will proceed with reference being made to preferred
9 embodiments and methods of use, the present invention is not intended to be limited
10 to these preferred embodiments and methods of use. Rather, the present invention is
11 of broad scope and is intended to be limited as only set forth in the accompanying
12 claims.

13 Other features and advantages of the present invention will become apparent
14 as the following Detailed Description proceeds, and upon reference to the Drawings,
15 wherein like numerals depict like parts, and wherein:

16 Brief Description of the Drawings

17 Figure 1 is a block diagram of an exemplary battery cell charging current
18 balancing circuit of the present invention;

19 Figure 2 is an exemplary circuit diagram of the battery cell charging current
20 balancing circuit of one embodiment of the present invention;

21 Figure 3 is an exemplary circuit diagram of the battery cell charging current
22 balancing circuit of another embodiment of the present invention;

23 Figure 4 depict additional details of the circuits of Figures 2 and 3;

24 Figure 4A depicts a plot of charge vs. voltage of a battery cell charged by the
25 circuits of Figures 2-4; and

26 Figure 5 is a flowchart of the bleeding current generation of the cell charging
27 current balancing circuit of the present invention.

28 Detailed Description of Exemplary Embodiments

29 Figure 1 is a block diagram of an exemplary cell balancing circuit of the
30 present invention. Essentially, the cell-balancing circuit 100 operates to control the
31 charge distribution among non-identical cells in a battery pack during the charge
32 process. The circuit monitors the voltage of each individual battery cell, Cell1,

1 Cell2...Celln, that are connected in series within the battery, and adjusts the amount
2 of charging current based on the cell voltage. The cells in a battery pack typically
3 present a certain degree of charge capacity imbalance. Therefore, in conventional
4 charging systems, the cells with a lower capacity will be charged faster than those
5 with a larger capacity. In such a condition, there is no way to achieve 100% charging
6 for all the cells in the battery, since either the larger capacity cells will remain
7 undercharged, thereby reducing the effective capacity of the battery, or the lower
8 capacity cells will be overcharged, with detrimental effects on long-term cell
9 reliability. Moreover, and especially with Lithium ion batteries, it is imperative that
10 an overcharge condition is not reached, since these batteries can be explosively
11 volatile at overcharged conditions. Accordingly, the present invention alleviates this
12 problem by dynamically varying the charge current supplied to each cell. The charge
13 controller 102 deflects a portion of the charging current that is supplied to each cell by
14 turning on the bleed current source 106, 108...110 for that cell, based on individual
15 cell voltage conditions. The bleed current source operates to bleed off a portion of the
16 charging current supplied to that cell. This is described in more detail below.

17 Figure 2 is a more detailed exemplary circuit diagram of the battery cell
18 charging current balancing circuit 200 of one embodiment of the present invention. It
19 should be noted at the outset that controller circuit 102' of Figure 2 is for a single cell.
20 Each cell in the battery would have a substantially identical circuit. In this example,
21 the controller, circuit 102' includes a transconductance amplifier 112 which controls
22 the value of a bleeder current I_{bl} . In this embodiment, the bleeder current I_{bl} is bled
23 directly from the total current I_{Ch} entering the cell.

24 At node 120, the charger 104 supplies a total charging current I_{Ch} . As the
25 voltage of the cell V_{cell} approaches a predetermined threshold reference value ($V_{100\%}$),
26 amplifier 112 generates I_{bl} to bleed off from the charging current $I_{charger}$ being
27 supplied to the cell. Thus, as a general rule, $I_{Ch} = I_{charger} + I_{bl}$. Generally, $V_{100\%}$
28 represents the voltage indicative of a fully charged battery, and may be programmably
29 specified by the battery or input into the controller 102' as one of the operating
30 parameters of the particular battery being charged. In a conventional battery, there
31 are typically 3 or 4 cells, but the present invention is generally applicable to any
32 number of cells. Additionally, the charge controller 102' includes a charging current

1 feedback loop that includes current generator 116 and comparator 118, which
2 generates a control signal to adjust the charging current I_{Ch} generated by charger 104.

3 It should be noted that the reference voltage $V_{100\%}$ and the reference current
4 I_{blmax} can be generated using constant voltage and current sources, respectively.
5 Alternatively, these signals may be generated using a programmable voltage and
6 current source. If, for example, the present invention is utilized in a Lithium ion
7 battery environment, it may be important that the reference voltage and current are
8 accurate to the third decimal place. Thus, it is preferable that $V_{100\%}$ and I_{blmax} are
9 generated having a tolerance of $\pm .001$ V. and $\pm .01 \mu A.$, respectively. Of course,
10 those skilled in the art will recognize that programmable voltage and current sources
11 are generally available, and all are deemed within the scope of the present invention.

12 In operation, amplifier 112 compares the battery cell voltage V_{cell} with a
13 predetermined maximum allowable charge voltage $V_{100\%}$. Preferably, amplifier 112 is
14 a transconductance amplifier having unitary output proportional to g_m . Amplifier 112
15 generates a bleeder current I_{bl} that is a function of $g_m (V_{cell} - V_{100\%})$. Based on the
16 recharge power requirement of the battery, charger 104 generates a charging current
17 I_{Ch} . Each cell receives a charging current $I_{Charging}$ which is a portion of the total I_{Ch} .
18 Each cell receives a charging current, $I_{Charging} = I_{Ch} - I_{bl}$. Since I_{bl} is determined for
19 each cell, it is possible with present invention to prevent the overcharge or fast charge
20 conditions, mentioned previously.

21 It is desirable that the total bleed current for each cell, I_{bl} , is set at some
22 maximum value. Accordingly, I_{bl} is compared to a maximum allowed bleeder
23 current. As shown in the figure, I_{bl} is compared to I_{blmax} 116, at comparator 118. The
24 output of comparator 118 generates a feedback signal to the charger circuit 104,
25 thereby setting the value of I_{Ch} . As I_{bl} approaches I_{blmax} , I_{Ch} will be reduced
26 accordingly.

27 Figure 3 depicts another exemplary circuit diagram of the battery cell charging
28 current balancing circuit 300 of another embodiment of the present invention. It
29 should be noted at the outset that controller circuit 102'' of Figure 3 is for a single
30 cell. Each cell in the battery would have a substantially identical circuit. Similar to
31 the previous embodiment, the controller circuit 102'' includes a transconductance
32 amplifier 112 which controls the value of a bleeder current I_{bl} . In this embodiment,

1 however, a current mirror 114 is provided which act as a current generator for the
2 bleeder current I_{bl} and as a current multiplier to generate $I_{bl} \times n$, where n represents an
3 arbitrary current multiplier, typically on the order of 10^3 . In this second embodiment,
4 the present invention minimizes power dissipation by recognizing that typically, the
5 bleeder current I_{bl} is non-usable power dissipation (i.e., waste current). Thus, it may
6 be preferable to generate a very small value bleeder current and multiply that value as
7 required for each cell. Since it may be preferable to implement the present invention
8 in an integrated circuit, power dissipation considerations and/or dissipation tolerances
9 must be recognized. Accordingly, the circuit 102'' of this embodiment utilizes a
10 multiple of the bleeder current, $I_{bl} \times n$, to act as the actual current bled from a cell. Of
11 course, this is only an example. For certain implementations it may not be necessary
12 or desirable to generate a bleeder current at all. Still other implementations may
13 require a multiple of a different arbitrary value. All such alternatives and
14 modifications are deemed within the scope of the present invention.

15 Otherwise, the operation of the circuit 102'' operates identically to the circuit
16 102' of Figure 2 except that $I_{bl} \times n$ is bled from the cell, rather than I_{bl} .

17 It is important to recognize, as depicted in greater detail in Figures 4 and 4A,
18 that in reality, a battery cell is viewed as an internal source V_I and a series internal
19 resistance R_I . The internal resistance is an unknown quantity (e.g., ranging from
20 approximately $50\text{m}\Omega$ to $200\text{m}\Omega$ for any given cell in a Lithium Ion battery), and can
21 vastly affect the true charge on the cell, since only the total cell voltage can be
22 monitored. Thus, it is equally important to devise a strategy to accurately charge a
23 cell based solely on the internal source, not the internal resistance. The total voltage
24 of the cell $V_{\text{cell-Total}}$ can be expressed as $V_{\text{cell-Total}} = V_I + V_{RI}$, where $V_I \gg V_{RI}$. Under
25 initial charging conditions, when a cell has not reached a maximum allowable voltage
26 ($V_{100\%}$) and there is therefore no bleeder current bled from that cell, $I_{ch} = I_{\text{charging}}$,
27 therefore, $V_{RI} = I_{ch} \times R_I$. When the voltage of the cell exceeds 100% ($V_{\text{cell}} > V_{100\%}$), a
28 bleeder current is drained from the cell, as described above. Therefore, $I_{\text{charging}} = I_{ch} -$
29 I_{bl} . Thus, I_{ch} has decreased, but the cell is still being charged, albeit at a slower rate,
30 i.e., V_I is increasing. Since $V_{RI} = I_{\text{charging}} \times R_I$, and I_{charging} has decreased, V_{RI} must
31 therefore decrease. (Since $V_I \gg V_{RI}$, it does not matter that V_{RI} decreases).

1 However, when $V_{\text{cell} - \text{Total}} > V_{100\%}$ (by some predetermined amount, e.g.,
 2 50mV), the charger changes state from a constant current source to a constant voltage
 3 source. In other words, charger 104 using feedback signal generated by comparator
 4 118 holds the voltage constant across the cell in this condition. Note that, under these
 5 conditions, $I_{bl} = I_{bl\text{max}}$, and now the charger changes I_{ch} to keep both the cell voltage
 6 constant and $I_{bl} = I_{bl\text{max}}$. Figure 3A depicts a graph the charge of the cell as a function
 7 of V_I . Recall that $I_{bl} = g_m (V_{\text{cell}} - V_{100\%})$, and likewise under these conditions $I_{bl} =$
 8 $I_{bl\text{max}}$, this condition forces the charger to keep $V_{\text{cell}} = V_{100\%} + I_{bl}/g_m$. But, $V_{\text{cell}} = V_I +$
 9 $I_{\text{charging}} \times R_i$, so when V_I increases I_{charging} decreases smoothly once the cell has
 10 reached capacity. Note that, according to the equation noted in Figure 4A, the rate of
 11 decrease will be smooth unless the internal series resistance changes.

12 Figure 5 depicts a flowchart 300 of the overall process of individual cell
 13 charging according to the embodiment of Figure 3. For clarity, reference numbers to
 14 the preferred components depicted in Figure 3 have been omitted. Initially, a
 15 charging current I_{ch} is supplied to the cell 302. Actually, since the cells are connected
 16 in series, I_{ch} is the current supplied to all the cells, however, the foregoing discussion
 17 will be in reference to a single cell, recognizing, of course, that an identical process
 18 occurs on all the cells. A measurement is made of the cell voltage V_{cell} 304. The cell
 19 voltage is compared to a threshold cell voltage, $V_{100\%}$ 306. It is then determined if
 20 $V_{\text{cell}} > V_{100\%}$ 308. If not, a charging current I_{charging} (not shown), proportional to I_{ch} is
 21 supplied to the cell for charging. If $V_{\text{cell}} > V_{100\%}$, a bleeder current, I_{bl} is generated,
 22 proportional to the amount that V_{cell} exceeds $V_{100\%}$ 310. In this embodiment, a
 23 multiple of the bleeder current, $I_{bl} \times n$ is generated 314. $I_{bl} \times n$ is bled from the cell
 24 318. The charging power to the cell is reduced accordingly, and the cell continues
 25 charging with $I_{\text{charging}} = I_{ch} - (I_{bl} \times n)$. At the same time, I_{bl} is compared with a
 26 maximum bleeder current, $I_{bl\text{max}}$ 316. It is determined if $I_{bl} > I_{bl\text{max}}$ 320. If not, steps
 27 210-316 continue ($I_{bl} \times n$ continues to be bled from the cell 318). If I_{bl} is greater than
 28 (or equal to) $I_{bl\text{max}}$, the charging current I_{ch} is set to ensure that the total cell voltage,
 29 $V_{\text{cell} - \text{Total}}$, remains constant (i.e., $I_{bl} = I_{bl\text{max}}$). Since the internal source of the cell is
 30 still charging (albeit at a much lower rate) the charging current I_{charging} is still supplied
 31 to the cell 326, but its value continually decreases (until conditions change).
 32 Accordingly, a continuous measurement is made of the cell voltage, 304 and the

1 process repeats, if necessary (i.e., V_{cell} is less than $V_{100\%}$). Since this process is
2 proscribed for each cell in the battery, it is ensured that all other cells that have yet to
3 reach maximum charging capacity receive a charging current of $I_{bl} \times n$, since if one
4 cell has reached its maximum the total charging current supplied by the charger is set
5 to I_{blmax} . A cell will reach capacity before other cells if either the cell has a smaller
6 capacity compared to other cells, or if the cell has a large internal resistance. The
7 present invention essentially factors out both of these imbalances between cells
8 thereby achieving active cell balancing of cells of different charging capacities and
9 different charging rates.

10 For the circuit 102' of Figure 2, the process is similar as described above,
11 except that in steps 314, 318 and 320, $I_{bl} \times n$ is replaced with I_{bl} . This value is used to
12 bleed current from the cell.

13 Thus, it is evident that there has been provided a cell balancing circuit that
14 satisfies the objectives stated herein. Numerous modifications and substitutions will
15 be recognized by those skilled in the art. For example, the charger circuit 104 can
16 include any known topology for generating a charging current for batteries, and
17 preferably is comprised of a single charge/discharge path topology, such as may be
18 found in U.S. Application Serial No. 09/624,918, entitled "Power Management
19 Circuit For Battery Systems", filed July 25, 2000 and assigned to the same assignee,
20 and hereby incorporated by reference in its entirety. Likewise, the current
21 mirror/multiplier circuit 114 can include any conventional and/or custom circuitry to
22 generate the aforementioned current signals.

23 Those skilled in the art will equally recognize that the transconductance
24 amplifier 112 can be replaced with equivalent circuits, to generate the proportional
25 bleeder current. To provide real-time cell status monitoring and adjustment, it is
26 preferable that the circuit topology 102' and 102'' shown in Figures 2 and 3 is an
27 analog, as shown. However, an equivalent digital circuit could be implemented using
28 the process depicted in Figures 2 and 3.

29 Still other modifications may be made. Although not shown in the figures, the
30 description above is duly described for multiple cells in a battery pack. To monitor
31 conditions on all the cells in a unified manner, it may be desirable to include have all
32 the feedback signals first fed into an OR gate, the output of which dictating the set

- 1 condition for the charger circuit. In this way, it is ensured that charging is balanced
- 2 among the cells. All such modifications are deemed within the scope of the present
- 3 invention, as defined by the appended claims.

CLAIMS

- 1
2 1. A battery cell charging circuit, comprising:
3 a charger circuit supplying a charging current to said battery cell;
4 a comparator for comparing a battery cell voltage to a predetermined threshold
5 cell voltage, said comparator controlling the generation of a bleeder current based on
6 the amount said battery cell voltage exceeds said predetermined threshold, said
7 bleeder being subtracted from said charging current supplied to said battery cell.
- 8 2. A circuit as claimed in claim 1, wherein said comparator comprising a
9 transconductance amplifier comparing said battery cell voltage to a predetermined
10 threshold voltage and controlling the generating said bleeder current as a function of
11 g_m .
- 12 3. A circuit as claimed in claim 1, further comprising a second comparator for
13 comparing said bleeder current to a maximum allowable bleeder current value, and
14 generating a feedback signal to said charger circuit to control the value of said
15 charging current.
- 16 4. A circuit as claimed in claim 3, further comprising a constant current source
17 generating said maximum allowable bleeder current value.
- 18 5. A circuit as claimed in claim 3, further comprising a programmable current
19 source for programmably generating said maximum allowable bleeder current value.
- 20 6. A circuit as claimed in claim 1, further comprising a constant voltage source
21 for generating said threshold cell voltage.
- 22 7. A circuit as claimed in claim 1, further comprising a programmable voltage
23 source for generating said predetermined threshold cell voltage.
- 24 8. A circuit as claimed in claim 1, wherein said battery comprises a lithium ion
25 battery, said charging current is approximately 2 Amps, and said predetermined
26 maximum cell voltage is approximately 4.200 Volts.
- 27 9. A circuit as claimed in claim 1, wherein said bleeder current is equal to about
28 $50\mu A$., and said multiple is equal to about 1000.
- 29 10. A method for charging a battery, comprising the steps of:
30 supplying a charging current to a battery cell;
31 comparing the battery cell voltage to a threshold cell voltage;

1 generating a bleeder current if said cell voltage exceeds said threshold cell
2 voltage; and

3 subtracting said bleeder current from said charging current.

4 11. A method as claimed in claim 10, wherein said step of generating said bleeder
5 current further comprises the step of multiplying said bleeder current by a
6 predetermined constant and subtracting the multiplied bleeder current from said
7 charging current.

8 12. A method as claimed in claim 10, further comprising the steps of:
9 comparing said bleeder current to a maximum allowable bleeder current value;
10 and

11 adjusting the value of said charging current if said bleeder current equals or
12 exceeds said maximum allowable bleeder current value.

13 13. A method as claimed in claim 12, further comprising the step of:
14 setting the bleeder current to equal the maximum allowable bleeder current
15 value when said bleeder current equals or exceeds said maximum allowable bleeder
16 current value, and subtracting said maximum allowable bleeder current from said
17 charging current.

18 14. A battery cell charging circuit, comprising a battery including a plurality of
19 cells; a charger circuit for supplying a charging current to each said cell; a first
20 comparator for comparing a battery cell voltage to a predetermined threshold cell
21 voltage, said comparator controlling the generating a bleeder current proportional to
22 the amount said battery cell voltage exceeds said predetermined threshold; a current
23 mirror for generating said bleeder current and a multiple of said bleeder current, said
24 multiple of said bleeder being subtracted from said charging current supplied to said
25 battery cell; and a second comparator for comparing said bleeder current to a
26 maximum allowable bleeder current value, and generating a feedback signal to said
27 charger circuit to control the value of said charging current.

28 15. A circuit as claimed in claim 14, wherein said comparator comprising a
29 transconductance amplifier comparing said battery cell voltage to a predetermined
30 threshold voltage and controlling the generating said bleeder current as a function of
31 g_m .

1 16. A circuit as claimed in claim 14, further comprising a constant current source
2 generating said maximum allowable bleeder current value.

3 17. A circuit as claimed in claim 14, further comprising a programmable current
4 source for programmably generating said maximum allowable bleeder current value.

5 18. A circuit as claimed in claim 14, further comprising a constant voltage source
6 for generating said predetermined threshold cell voltage.

7 19. A circuit as claimed in claim 14, further comprising a programmable voltage
8 source for generating said predetermined threshold cell voltage.

9 20. A circuit as claimed in claim 14, wherein said battery comprises a lithium ion
10 battery, said charging current is approximately 2 Amps, and said predetermined
11 maximum cell voltage is approximately 4.200 Volts.

12 21. A circuit as claimed in claim 14, wherein said bleeder current is equal to about
13 50 μ A., and said multiple is equal to about 1000.

1/5

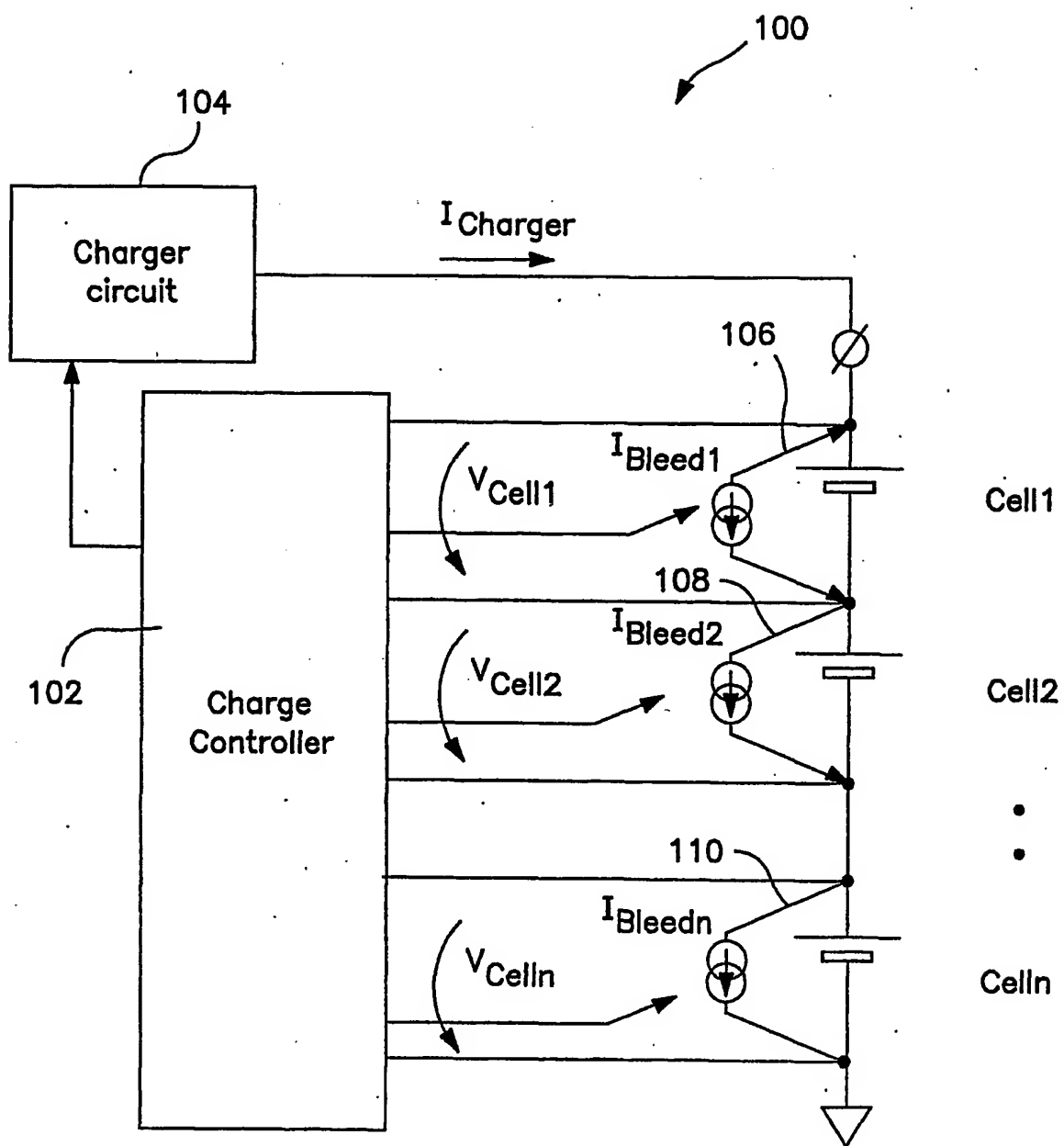


FIG. 1

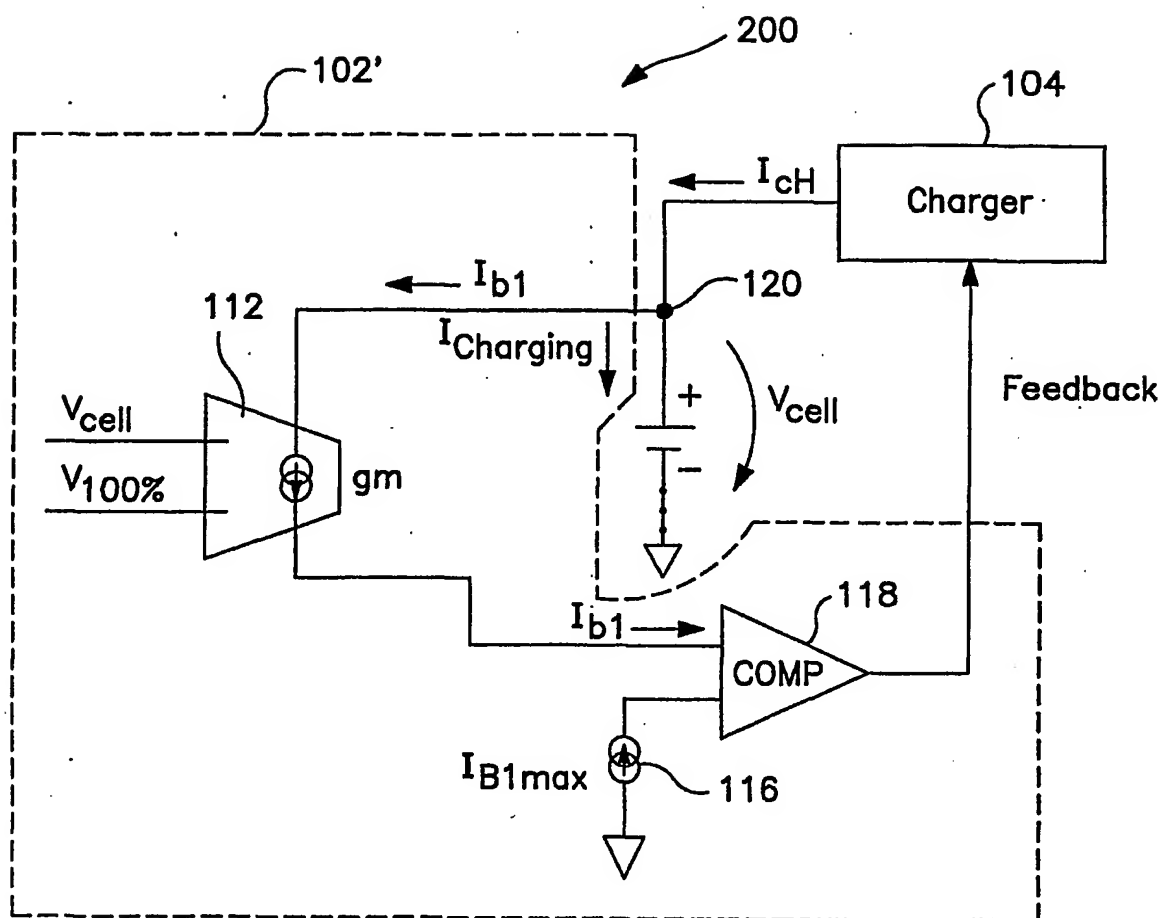


FIG. 2

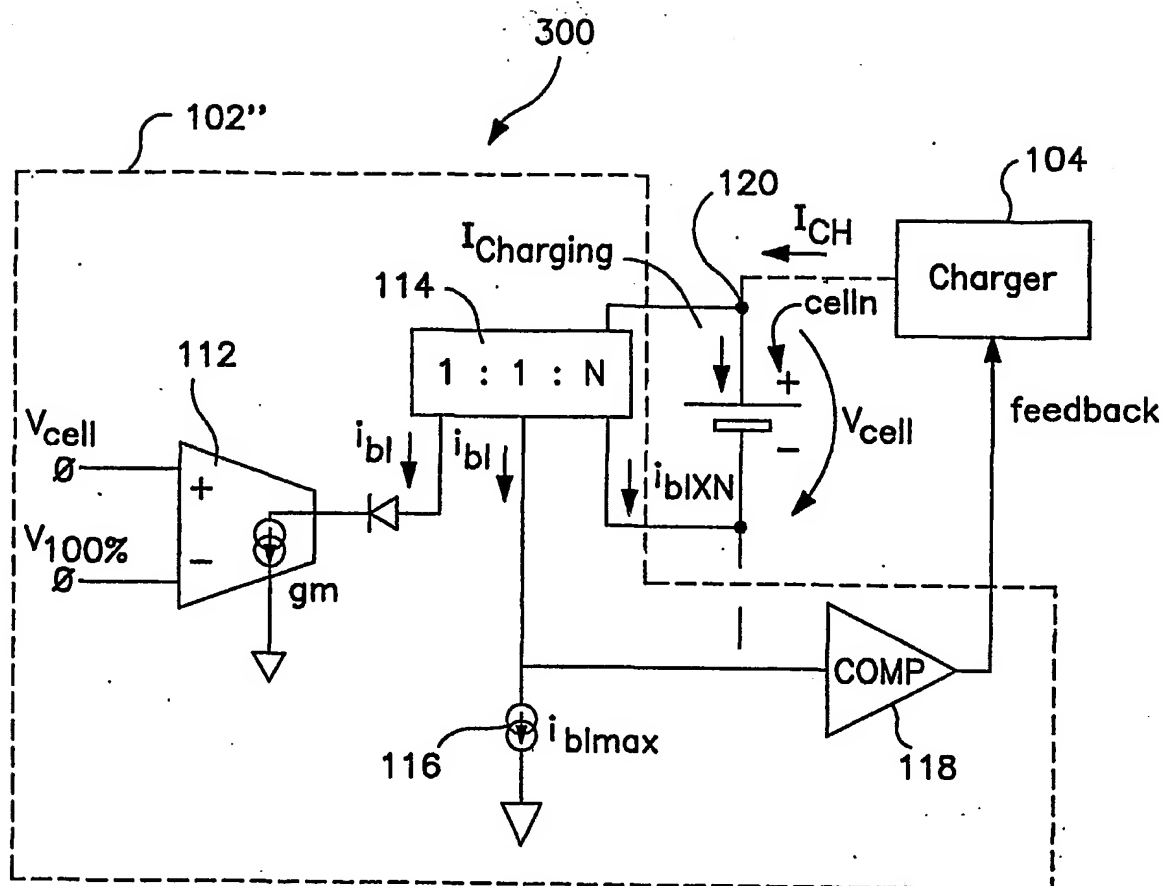


FIG. 3

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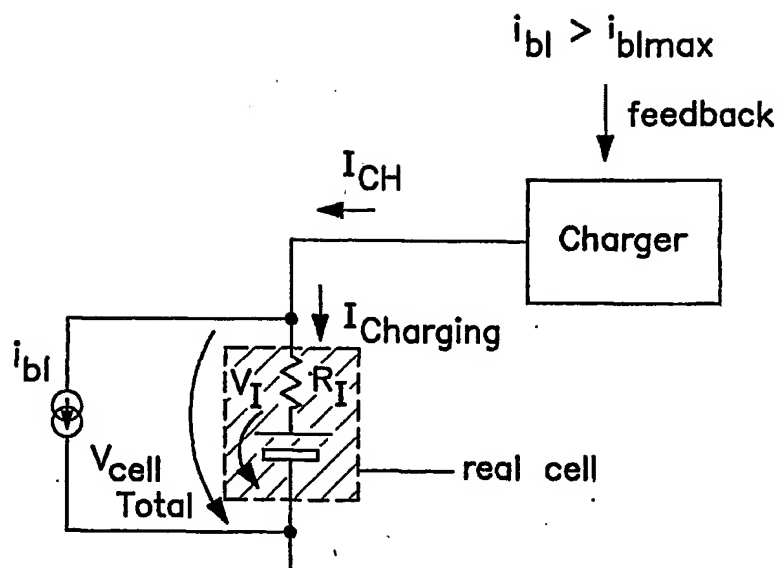


FIG. 4

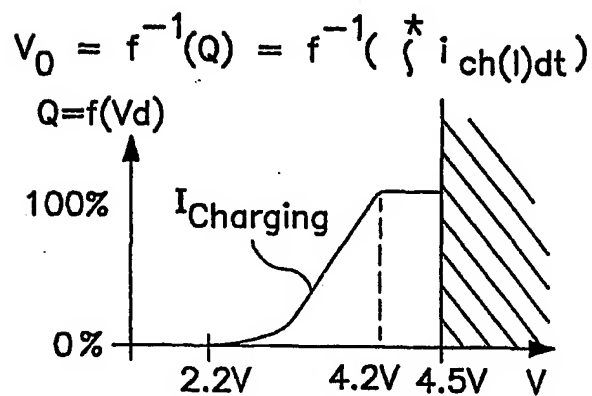


FIG. 4A

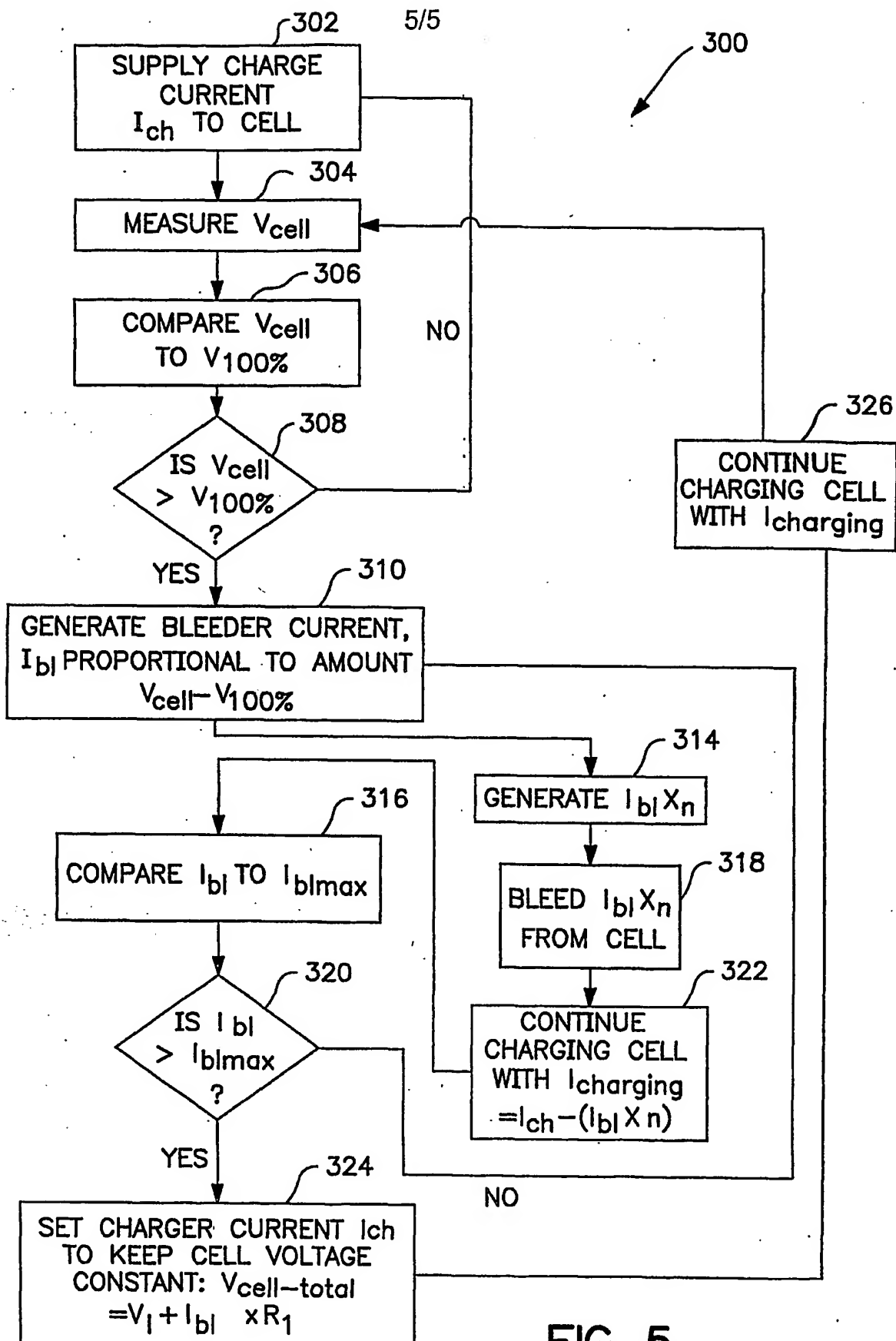


FIG. 5

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US01/27637**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(7) :H01M 10/44, 10/46

US CL :320/118

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 320/116-122

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X --- A	US 5,592,067 A (PETER et al.) 07 JANUARY 1997 (07.01.97) see abstract and figure 1.	1, 3-7, 10, 12, 13 ----- 2, 8, 9, 11, 14-21

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	
"A" document defining the general state of the art which is not considered to be of particular relevance	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"E" earlier document published on or after the international filing date	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"O" document referring to an oral disclosure, use, exhibition or other means	"&" document member of the same patent family
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

14 NOVEMBER 2001

Date of mailing of the international search report

26 DEC 2001

Name and mailing address of the ISA/US
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